

14. KAMENYARZH YA.A., Stresses in incompressible media. Equivalence of formulations of ideal plasticity problems. Dokl. Akad. Nauk SSSR, 261, 1, 1981.
15. KAMENYARZH YA.A., On formulations of the problems of ideal plasticity theory, PMM, 47, 3, 1983.
16. MOSOLOV P.P. and MYASNIKOV V.P., Mechanics of Rigidly Plastic Media. Nauka, Moscow, 1981.
17. SEREGIN G.A., Expansion of the variational formulation of the problem for a rigidly plastic medium to a velocity field with slip type discontinuities, PMM, 47, 6, 1983.
18. KAMENYARZH YA.A., Statically allowable stress fields in incompressible media, PMM, 47, 2, 1983.
19. TEMAM R. and STRANG G., Duality and relaxation in the variational problems of plasticity, J. Meč., 19, 3, 1980.

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## ON ASYMPTOTIC INTEGRATION OF THE EQUATIONS OF MOTION OF MECHANICAL SYSTEMS SUBJECTED TO RAPIDLY OSCILLATING FORCES\*

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An algorithm for the direct expansion of solutions of the Cauchy problem in a small parameter in a finite time interval is proposed in the development of the idea in the author's paper /1/ for systems of differential equations describing the motion of mechanical systems subjected to rapidly oscillating forces.

We consider a mechanical system whose motion is described by the vector differential equation

$$A(q)q'' + B(q)q' = F(t, q) + \omega\Phi(t, q, \tau) \quad (1)$$

where  $q = (q^1, \dots, q^n)$  is the generalized coordinate vector, the dot denotes differentiation with respect to time  $t$ ,  $A$  is a positive-definite matrix of the inertial forces,  $B$  is the matrix of the dissipative forces,  $\omega\Phi$  are large amplitude oscillating forces ( $\omega \gg 1$ ,  $\tau = \omega t$ ). For simplicity we will consider  $\Phi$  to be a trigonometric polynomial in  $\tau$  of period  $2\pi$ , with zero mean in  $\tau$ . Let the following initial conditions be given

$$q(0) = \alpha, \quad q'(0) = \beta \quad (2)$$

We will seek the approximate solution of the Cauchy problem (1) and (2) in the form

$$q^* = u_0(t) + \omega^{-1}[u_1(t) + v_1(t, \tau)] + \dots + \omega^{-s}[u_s(t) + v_s(t, \tau)] + \dots \quad (3)$$

where  $v_i(t, \tau)$  are periodic functions of  $\tau$  of period  $2\pi$  with zero mean value. The sum  $u_0 + \omega^{-1}u_1 + \dots$  is the smooth motion component while  $\omega^{-1}v_1 + \omega^{-2}v_2 + \dots$  is the vibrational component. We have

$$\begin{aligned} A(q^*) &= A^0 + \omega^{-1}A_q^0(u_1 + v_1) + \\ &\omega^{-2}A_q^0(u_2 + v_2) + \frac{1}{2}\omega^{-2}A_{qq}^0(u_1 + v_1)^2 + \dots \\ (A^0 &= A(u_0), \quad A_q^0 = A_q(u_0), \dots) \end{aligned}$$

Analogous expressions hold for  $B(q^*)$ ,  $F(t, q^*)$ ,  $\dots$ .

We obtain from the initial conditions (2), formulas (3) and the result of differentiating (3) with respect to  $t$

$$\begin{aligned} u_0(0) + \omega^{-1}[u_1(0) + v_1(0,0)] + \omega^{-2}[u_2(0) + v_2(0,0)] + \dots = \alpha \\ u_0'(0) + \partial v_1(0,0)/\partial\tau + \omega^{-1}[u_1'(0) + v_1'(0,0)] + \partial v_2(0,0)/\partial\tau + \dots = \beta \end{aligned} \quad (4)$$

It therefore follows that

$$u_0(t) = \alpha, \quad u_0'(0) + \partial v_1(0,0)/\partial\tau = \beta \quad (5)$$

while the coefficients for  $\omega^{-1}, \omega^{-2}, \dots$  in expansions (4) are zero. Now substituting (3) into (1), we obtain the identity

$$A(q^*)q^{**} + B(q^*)q^* = F(t, q) + \omega\Phi(t, q^*, \tau) \quad (6)$$

We try to select  $u_i$  and  $v_i$  such that the identity (6) would be satisfied for all  $x \in [0, T]$  and  $\tau \in [0, \infty)$ . We equate the coefficients of powers of  $\omega, \omega^0, \omega^{-1}, \omega^{-2}, \dots$ , etc.

We obtain for the first power in  $\omega$

$$A^0 \partial^2 v_1 / \partial \tau^2 \equiv \Phi^0 \quad (\Phi^0 = \Phi(t, u_0, \tau))$$

Since the matrix  $A^0$  is reversible and  $\Phi^0$  is a trigonometric polynomial in  $\tau$  with zero mean, then  $v_1$  can be determined uniquely in the form of a trigonometric polynomial in  $\tau$  with coefficients dependent on  $t$  and  $u_0$

$$v_1 = f_1(t, u_0, \tau) \quad (7)$$

If it is taken into account that  $u_0(0) = \alpha$ , then the quantity

$$\Psi_1(\alpha) = \partial v_1(0,0)/\partial\tau = \partial f_1(0, \alpha, 0)/\partial\tau$$

is completely determined. Consequently  $u_0'(0) = \beta - \Psi_1(\alpha)$  is also determined from (5).

Now equating coefficients for the zeroth power of  $\omega$  in the identity (6), we obtain

$$\begin{aligned} A^0 [u_0'' + 2\partial v_1'/\partial\tau + \partial^2 v_1/\partial\tau^2] + A_q^0 (u_1 + v_1) \partial^2 v_1/\partial\tau^2 + \\ B^0 (u_0' + \partial v_1'/\partial\tau) = F^0 + \Phi_q^0 (u_1 + v_1) (F^0 = F(t, u_0)) \end{aligned} \quad (8)$$

Let us calculate the mean value of the left and right sides of the last equality with respect to  $\tau$ . We have ( $W^0$  is the vibrational force)

$$\begin{aligned} A^0 u_0'' + B^0 u_0' \equiv F^0 + W^0 \\ W^0 = \langle \Phi_q^0 v_1(t, \tau) \rangle - \langle [A_q^0 v_1(t, \tau)] \partial^2 v_1/\partial\tau^2 \rangle \end{aligned} \quad (9)$$

Therefore, we obtain (9) and the initial conditions  $u_0(0) = \alpha$ ,  $u_0'(0) = \beta - \Psi_1(\alpha)$  to determine  $u_0(t)$ . We assume this problem to be solved in the segment  $[0, T]$ . Then we finally also obtain  $v_1(t, \tau)$  from (7).

We now examine components with zero mean in  $\tau$  in (8). We obtain

$$A^0 \partial^2 v_2/\partial\tau^2 = Q_1^0 + Q_2^0 u_1 \quad (10)$$

where  $Q_1^0$  and  $Q_2^0$  are known vector functions and matrices dependent on  $t, u_0, \tau$ . We will seek the function  $v_2$  in the form

$$v_2 = w_2(t, \tau) + Z_2(t, \tau) u_1(t)$$

where  $w_2(t, \tau)$  is a vector function while  $Z_2(t, \tau)$  is a matrix whose coefficients are trigonometric polynomials in  $\tau$  having zero mean value. Now  $w_2$  and  $Z_2$  are determined uniquely from (10), but, the function  $v_2$  still remains undetermined since the function  $u_1(t)$  is undetermined.

We now equate the coefficients for  $\omega^{-1}$  in (6) and in the equality obtained we take the average with respect to  $\tau$ . Consequently we obtain the following equation for  $u_1$

$$A^0 u_1'' + B^0 u_1' = d_1(t) + C_1(t) u_1 \quad (11)$$

where the vector function  $d_1(t)$  and the matrix  $C_1(t)$  are determined just by using the  $u_0, v_1, w_2$  and  $Z_2$  already known. Let us note that we conclude from the expression in square brackets in (4) being equal to zero that the quantities

$$u_1(0) = -v_1(0,0), \quad u_1'(0) = -v_1'(0,0) - \partial v_2(0,0)/\partial\tau \quad (12)$$

are known. This enables  $u_1$  to be determined completely from (11) and (12).

Furthermore,  $v_3$  should be sought in the form

$$v_3 = w_3(t, \tau) + Z_3(t, \tau) u_2(t)$$

etc. This procedure enables us to determine the approximate solution

$$q_N^* = u_0(t) + \omega^{-1}[u_1(t) + v_1(t, \tau)] + \dots + \omega^{-N}[u_N(t) + v_N(t, \tau)] \quad (13)$$

to any accuracy for any integer  $N \geq 1$ .

If the rapidly oscillating forces are not large and (1) has the form

$$A(q)q'' + B(q)q' = F(t, q) + \Phi(t, q, \tau)$$

then the approximate solution is found in the form (13) where  $v_1(t, \tau) \equiv 0$ .

## REFERENCES

1. STRYGIN V.V., On a modification of the averaging method for seeking high approximations. *PMM*, 48, 6, 1984.

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ON THE MITCHELL PROBLEM OF THE MOTION OF A LUBRICANT IN A LAYER BOUNDED  
BY A MOVING PLANE AND A FIXED PLATE OF FINITE SIZES\*

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The Reynolds equation which appears in the hydrodynamic theory of lubrication is applied to the case of the flow of a lubricant between a plane and an inclined plate, and is solved with help of the special functions for a rectangular as well as segmented form of the plate.

1. An unbounded plane moves longitudinally with velocity  $U$  in the direction of the  $x$  axis. We direct the  $y$  axis towards the liquid. Let  $h$  be the thickness of the layer, depending only on the coordinate  $x$ ,  $q = h_2/h_1 > 1$  the ratio of the thicknesses of the layer at the plate edges along the  $x$  axis,  $a$  the distance between these edges and  $2l$  the width of the plate in the direction of the  $z$  axis.

Using the well-known approximate Reynolds equation, we arrive at the following boundary value problem for the pressure:

$$\frac{\partial}{\partial x} \left( h^3 \frac{\partial p}{\partial x} \right) + h^3 \frac{\partial^2 p}{\partial z^2} = 6\mu U \frac{\partial h}{\partial x} \quad (1.1)$$

$$\begin{aligned} -l < z < l, \quad x = 0, \quad p = p_a; \quad x = a, \quad p = p_a \\ 0 < x < a, \quad z = \pm l, \quad p = p_a \end{aligned} \quad (1.2)$$

Since  $h$  depends only on  $x$ , it follows that a particular solution of Eq.(1.1) can be taken in the form

$$p_0 = \chi_0(x) = 6\mu U \int h^{-2} dx + C_1 \int h^{-3} dx + C_2 \quad (1.3)$$

We shall construct the solution of the corresponding homogeneous equation in the form  $p_n = \text{ch}(nz) \chi_n(x)$ . In this case we obtain the following equation for  $\chi_n$ :

$$\frac{d}{dx} \left( h^3 \frac{d\chi_n}{dx} \right) + n^2 h^3 \chi_n = 0 \quad (1.4)$$

whose complete solution will consist of two independent solutions  $\chi_n^{(1)}$  and  $\chi_n^{(2)}$ , so that  $\chi_n = A_n \chi_n^{(1)} + B_n \chi_n^{(2)}$ .

We can show in the usual manner that the functions  $\chi_n$  are orthogonal

$$\int_0^a \chi_m \chi_n h^3 dx = 0, \quad m \neq n \quad (1.5)$$

when the following conditions hold:

$$A_n \chi_n^{(1)}(0) + B_n \chi_n^{(2)}(0) = 0, \quad A_n \chi_n^{(1)}(a) + B_n \chi_n^{(2)}(a) = 0 \quad (1.6)$$

Combining the particular solution (1.3) with the set of solutions  $\chi_n$ , we obtain the general solution of Eq.(1.1) in the form

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